

Pores distribution statistical analysis for metal foams obtained by casting-dissolution process

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ABSTRACT

Interesting properties of metal foams such as light weight, good energy absorption and low thermal conductivity, have promoted the development of new processes to improve properties without sacrificing productivity. This study aims to verify the uniformity pore distribution in an aluminum alloy foam obtained by Casting - Dissolution Process, using a nondestructive analysis. In order to evaluate mechanical properties of a metal foam using computational numerical models, the use of a small reconstructed section of the sample representing an entire volume of metal foam, was validated. In conclusion, it was possible to determine that all parts of the sample have the equivalent superficial area and volume.

Keywords: Metal foam, casting and dissolution process, porosity.

1. INTRODUCTION

Metal foams have several remarkable properties that make them suitable for many engineering uses. They are frequently used in different fields such as lightweight sandwich manufacturing, packaging and crashworthiness, because of their energy dissipation capability and their thermal and acoustical properties, which are still under study [1][2][3][4].

Different methods are proposed to get porous metals, starting from vapor phase on polymeric preforms, metal powder mixed with foaming agents, electrodeposited from an aqueous solution, injecting gas in the liquid metal or metal casting and infiltration on preforms [4][5]. It is known that the properties of metal foam and other cellular metal structures depend on the properties of the bulk metal as well as the homogeneity of the structural features such as: cell topology, relative density, cell size, cell shape and anisotropy, which in turn depend on the manufacturing method [6][7].

Several authors had shown limited number of methods to produce open cellular structures that allow obtaining uniform pore distribution. Zhao, *et al.* [8], developed the lost carbonate sintering process (LCS) for manufacturing metal foams with space holder technique and evaluated the cell structure using a visual analysis with SEM micrographs. They found the foam exhibits uniformly distributed open cells. Surace, *et al.* [7] implemented the Sintering-Dissolution Process (SDP), another space holder technique that uses water-soluble materials that allow controlling the cell shape, cell size and porosity. They measured the morphological parameters in a 2D cross section by an image software tool from the obtained samples that were longitudinally sawed cut with diamond blade [7].

Both, the foam structure and the pore morphology, depend on the fabrication method. In general, the SDP technic produces homogeneous foams, but it has not been established if every obtained sample has uniformly distributed pores, in a way that it can be concluded that a small portion of the sample is representative for all the volume in the mechanical response as well as in its geometry.

Thus, the aim of this work is to verify the pore distribution uniformity in an aluminum alloy foam obtained by Casting - Dissolution Process, using a nondestructive analysis, in order to validate the use of a small reconstructed section of the sample like a representative volume to evaluate mechanical properties of the metal foam using computational numerical models.

2. MATERIALS AND METHODS

2.1 Metal foam samples processing

Casting-Dissolution Process was used to manufacture the aluminum foams. To make the preform, NaCl particles were sieved to obtain controlled sizes of 2.0 mm, 1.0 mm and 0.5 mm, then they were put into a cylindrical steel mold, and finally were infiltrated with the AlSiMg liquid aluminum alloy under vacuum pressure and at temperature of 700°C. Al/NaCl composites of 10 cm in diameter and 8 in height were obtained. In order to reveal the porous structure, the salt was removed by water. This manufacturing method allows the porous to be present in all direction and with irregular shape replicated from the NaCl particles; so there is an inherent complexity in the structure geometry, where the porous are uniform but with random distribution.

2.2 Visualization, segmentation and morphometry

Different methods of visualization, segmentation and morphometry to analyze the geometry of foams are available. Due to the cell structure damage could be caused using destructive test, it was decided to do a nondestructive technique that allows to acquire detailed, quantitative, geometric datas from the three samples. X-ray micro-computed tomography (μ CT) was employed to obtain the required images.

The μ CT system used for the tomography of each sample consisted of a micro-focus 150 kV Hamamatsu X-ray source with a tungsten target and a flat panel detector C7942. A 100 kV filament voltage and a current of 100 μ A were used. Using a source-sample distance of 77.5 mm and a source-detector distance of 298 mm, it was achieved a magnification factor of 3,8 and a pixel size 13 mm. Additionally, the aluminum foams structure was examined by optical microscopy (Leica DMLM) and scanning electron microscope (JEOL JSM-6490LV SEM) to evaluate how the cells are interconnected.

Recent observations using X-ray μ CT showed up the feasibility of the 3D reconstruction and basic measurements on X-ray tomography and prove that this technique is suitable for the investigation of the microstructure of foams, because it enables to obtain a real image of the inside [9],[10].

The X-ray μ CT images were manipulated using specialized software, Mimics®, from which geometric information including strut length and pore shapes were extracted. Figure 1a. shows the 3D reconstruction from μ CT and the Fig 1b. the SEM image for one of the samples.

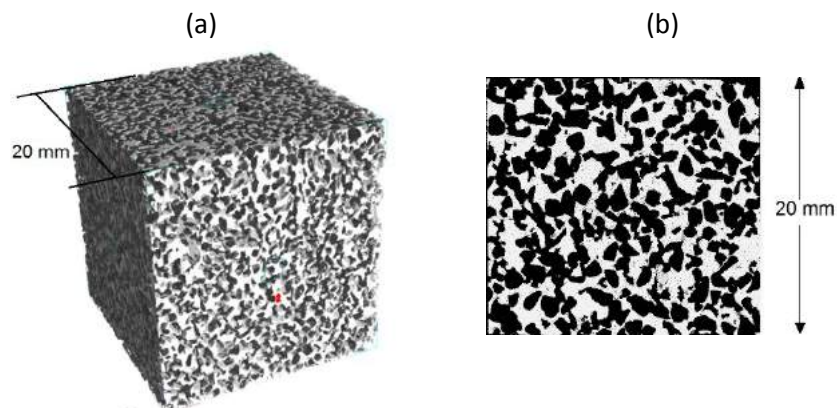


Figure 1: Sample with 0.5 mm pore size: (a) 3D reconstruct using Mimics® Materialise (b) Sample from SEM

2.3 Porous distribution analysis

As mentioned before, the major parameters to characterize the architecture of a cellular material are the global density and its fluctuation in the sample, the cell size distribution and the wall thickness distribution. In this sense, to determine if every obtained sample has uniformly distributed pores, a section of 99 μ CT image from each sample was imported to a 3D reconstruction using image analysis software, Mimics®.

The reconstruction of the solid pore interface allows to extract every morphological three dimensional parameter: volume, surface area, aspect ratio, sphericity [9] and a comparison of these measures in every sample will allow to determine if homogeneity exist. In this work, given the geometrical complexity of the cells, the aspect ratio and sphericity of the pores was not measured, and instead of that, the volume and surface area of every metallic foam sample were obtained.

The total analyzed images represent a volume of 20mm x 20mm x 10mm, a half of the actual size of the sample. Since the prime purpose is to obtain a minimum meshed volume able to be representative of the foam, the μ CT slices were sectioned looking for a rectangular region that at least has a completed and defined pore. Using crop tool, the sample with 0.5mm and 1.0 mm cell size were segmented into sixteen (16) parts, as shown in Figure 2, and four samples with 2.0mm cell size were segmented into five (5) parts carrying out the same purpose, as shown in Figure 3.

Once the 3D reconstruction of every box section was made, the surface area and volume were measured using Mimics measure tools and from each parameter an average was calculated.

An experiment was designed to compare the homogeneity of every box section for each cell size and was implemented using Minitab® software. The experimental factor was the foam zone and the experimental response variables for the Analysis of Variance (ANOVA) were surface area and volume. Experimental factor (foam zone) was divided in three levels: 1 (corners), 2 (boundaries), 3 (center), for 0.5mm and 1.0mm cell size as shown in Figure 2. The experiment has more than one replicate for each level. Further, foam zone of 2.0mm cell size was divided in five levels as in Figure 3. This segmentation ensures that there is at least one completed and defined pore in each part. Four 3D reconstruction of metal foam pore size 2.00 mm were carried out to ensure three replicates for each level.

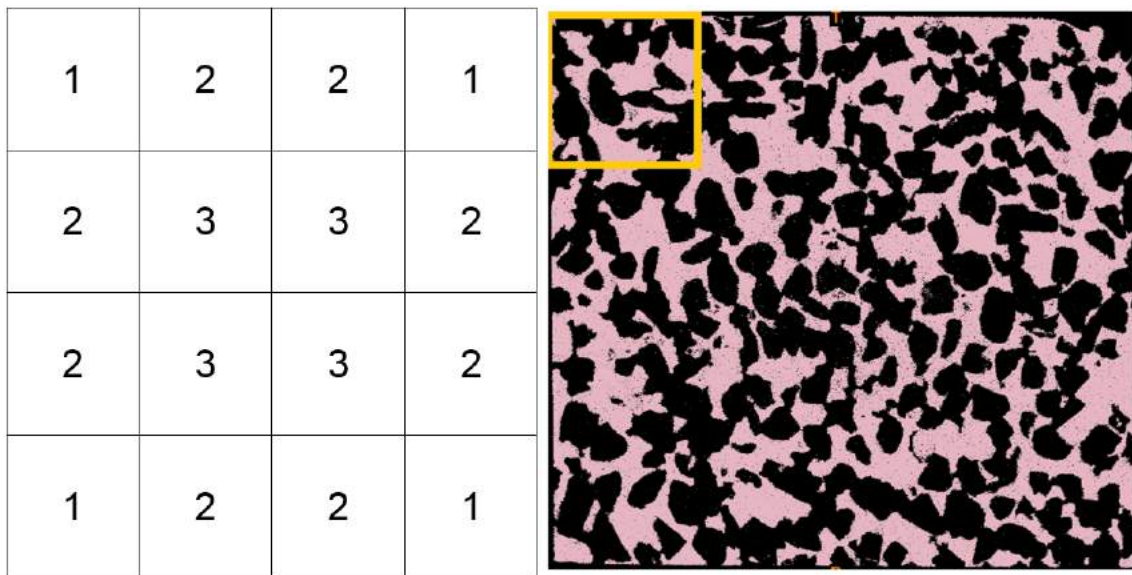


Figure 2: Sample segmentation foam with 1mm cell size.

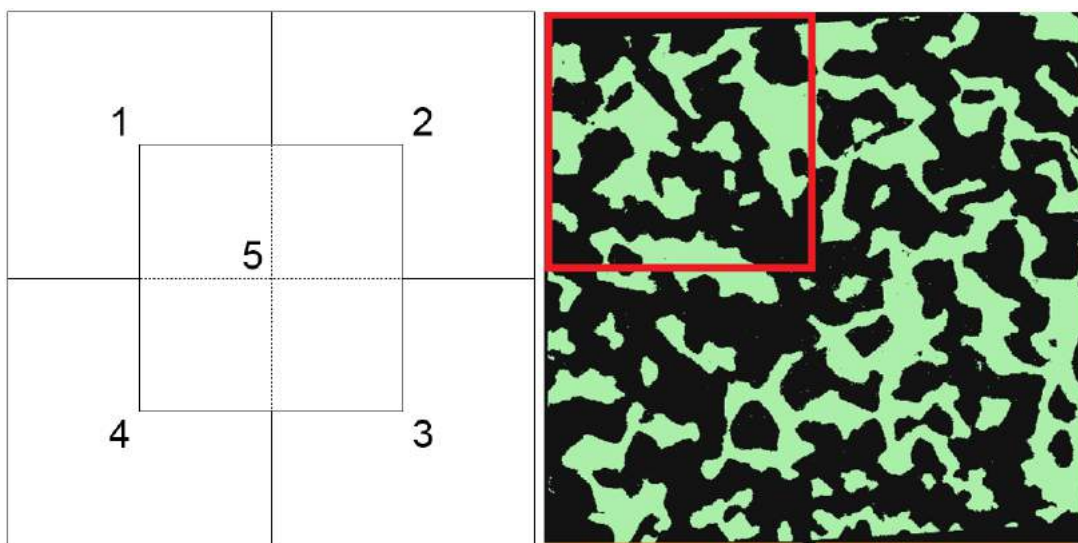


Figure 3: Sample segmentation foam with 2.0 mm cell size.

3. RESULTS

Taking into account the benefits of the non-destructive test to probe complex porous structures, this study goes beyond using 3D reconstruction in order to get every morphological three dimensional parameter. It allows to acquire detailed, quantitative, geometric data from the three samples.

As shown in Figure 4, the reconstructed samples show that foams exhibit well-interconnected open cells. The pores have extensive elongation with a uniform distribution without accumulation in few regions.

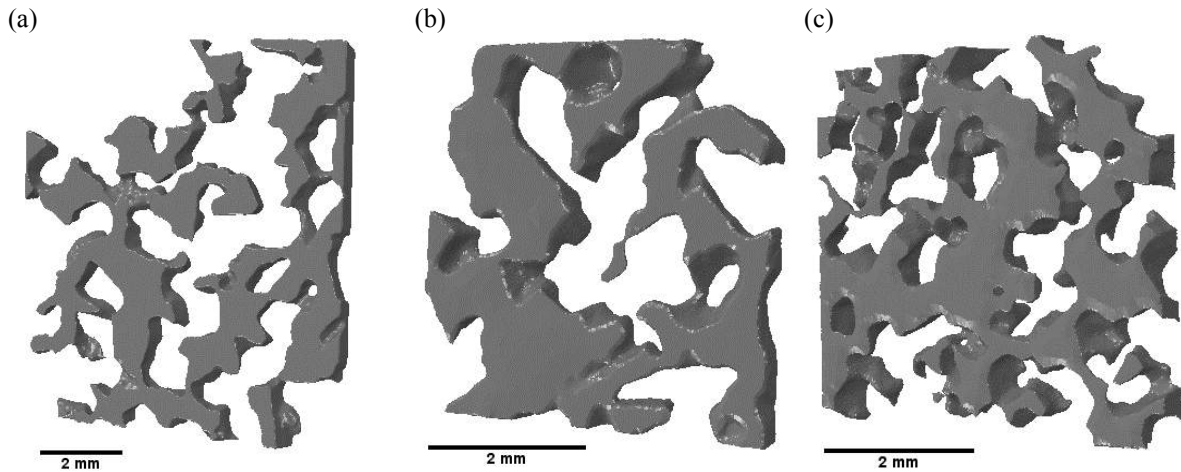


Figure 4: Reconstructed sample with (a). 2.0mm cell size, (b). 1.0mm cell size and (c). 0.5mm cell size.

In addition, a visual inspection of the μ CT shows that the obtained cell shape differs markedly from foams made by other methods starting from powders, as showed by B. H. Smith [4] in the micro-structure sample made by oxide ceramic foam precursor and made by powder metallurgy.

. Experiment design for 0.5mm cell size can be observed in Table 1. The experiment response variables were surface area and volume for each sample (0.5mm, 1.0 mm and 2.0mm cell size), percentage difference is the comparison between the foam zone section area and volume with the average from each sample. In addition, Table 2 and Table 3 shows examples of ANOVA for 0.5mm cell size, the first one has as response volume and the second one has surface area. From the analysis of variance (ANOVA) made with Minitab® it can be concluded that none of the factor levels are significant. The p-value reported is less than 0.05 for confidence percentage of 95%, this means that there is no statistical evidence that shows no homogeneity in the foam. Additionally, box and whisker graphs shown in Figure 5 are useful for comparing groups of data and prove that there is not effect of foam zone. The assumptions of normal distribution, equal variances, and randomization of the residuals were checked to guarantee the validity of the experiment conclusions, respective graphs are shown in the Figure 6 and Figure 7.

Table 1: Volume, superficial area and percentage difference of the 0.5 mm cell size sample.

FOAM ZONE	VOLUME [mm ³]	AREA [mm ²]	VOLUME PER- CENTAGE DIF- FERENCE	AREA PERCENTAGE DIFFE- RENCE
3	1,376,994	420,563	2%	1%
3	1,347,223	434,024	4%	2%
2	1,374,366	446,878	2%	5%
2	1,489,473	426,429	6%	0%
2	1,364,214	414,161	3%	3%
2	1,431,615	409,879	2%	4%
2	1,477,308	424,924	5%	0%
3	1,351,833	413,844	4%	3%

2	1,524,831	424,946	9%	0%
1	1,415,271	447,563	1%	5%
1	1,416,070	436,134	1%	3%
1	1,222,860	409,974	13%	3%
3	1,473,876	436,016	5%	3%
2	1,337,973	406,492	5%	4%
1	1,482,484	436,419	6%	3%
2	1,333,099	408,249	5%	4%

Table 2: One-way ANOVA: Volume versus Foam zone.

SOURCES	DEGREE OF FRE- EDOM	SUM OF SQUA- RES	MEAN SQUARES	FO	P - VALUE
Foam zone	2	3,812,363,001	1,906,181,500	0.29	0.756
Error	13	86,755,014,663	6,673,462,666		
Total	15	90,567,377,664			

Table 3: One-way ANOVA: Area versus Foam zone.

SOURCES	DEGREE OF FRE- EDOM	SUM OF SQUA- RES	MEAN SQUARES	FO	P - VALUE
Foam zone	2	411,432,113	205,716,057	1.13	0.354
Error	13	2,373,939,890	182,610,761		
Total	15	2,785,372,004			

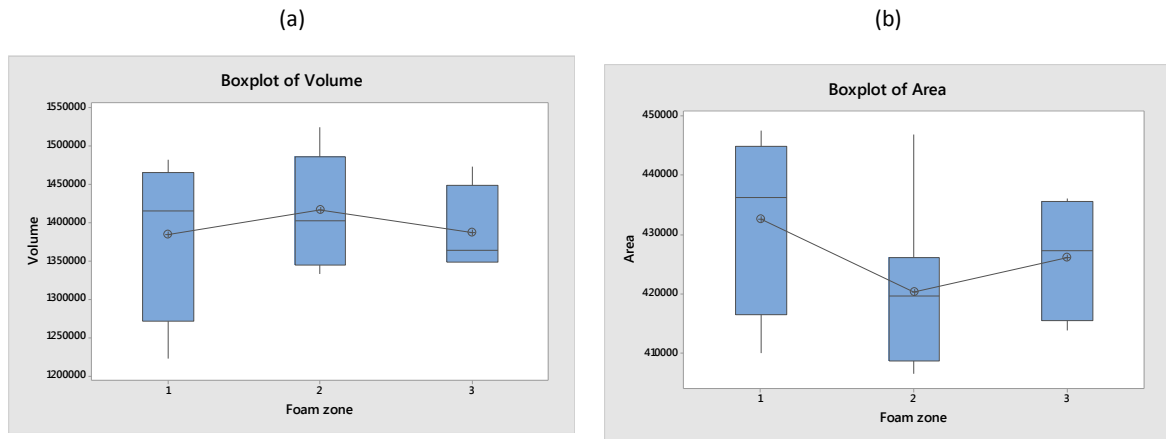


Figure 5: Box and whisker graphs: (a). Boxplot of Volume and (b). Boxplot of Area

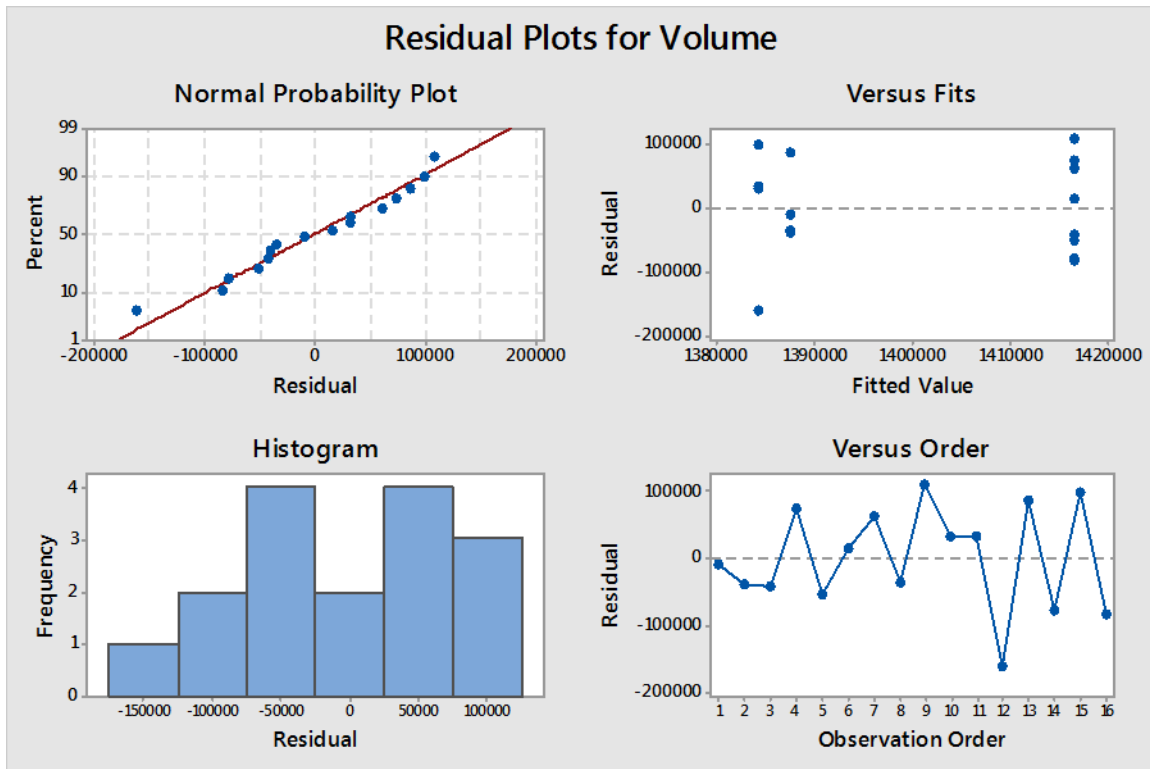


Figure 6: Residual plots for volume.

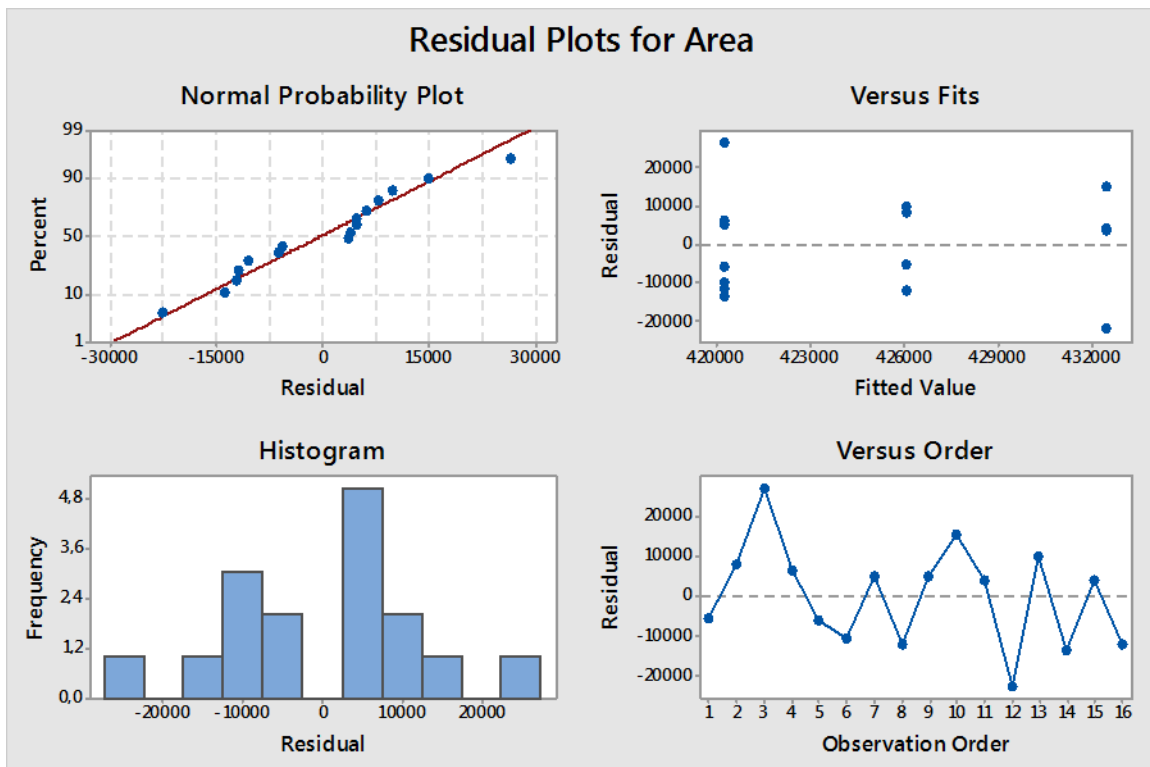


Figure 7: Residual plots for area.

Table 4 and Table 5 show experiment designs for 1mm and 2mm cell sizes, respectively. The assumptions of normal distribution, equal variances, and randomization of the residuals were checked to guarantee the validity of the experiment conclusions. Table 6 presents a summary of statistical analysis, where results show that all means are equal with a significance level $\alpha = 0,05$. As a result, there is no

statistical evidence that shows no homogeneity in the foam.

Table 4: Volume, superficial area and percentage difference of the 1.0 mm cell size sample..

FOAM ZONE	VOLUME [mm ³]	AREA [mm ²]	VOLUME PER-CENTAGE DIFFERENCE	AREA PERCENTAGE DIFFERENCE
1	1,381,437	273,793	2%	4%
2	1,427,444	265,326	1%	7%
2	1,674,686	273,444	18%	4%
2	1,396,061	284,243	1%	0%
2	1,347,892	264,490	5%	7%
2	1,489,908	302,619	5%	7%
3	1,394,344	297,361	1%	5%
1	1,362,803	265,482	4%	6%
2	1,355,965	267,758	4%	6%
3	1,399,169	293,909	1%	4%
3	1,420,846	296,198	0%	4%
2	1,493,212	293,524	6%	3%
3	1,418,221	292,444	0%	3%
2	1,375,053	300,427	3%	6%
1	1,407,497	309,392	0%	9%
1	1,277,335	260,459	10%	8%

Table 5: Volume, superficial area and percentage difference of the 2.0 mm cell size sample..

FOAM ZONE	VOLUME [mm ³]	AREA [mm ²]	VOLUME PER-CENTAGE DIFFERENCE	AREA PERCENTAGE DIFFERENCE
3	5,942,603	856,090	4%	3%
4	6,392,855	823,117	12%	1%
4	5,772,441	796,834	1%	4%
4	5,879,794	930,776	3%	12%
5	5,657,577	860,088	1%	3%
1	5,279,422	831,757	7%	0%
1	5,933,495	863,018	4%	4%
2	5,413,087	860,690	5%	3%
2	5,148,404	802,194	10%	4%
4	4,704,339	700,987	18%	16%
1	5,542,439	846,233	3%	2%
3	6,126,942	796,116	7%	4%
3	5,416,844	842,066	5%	1%
5	5,814,134	823,313	2%	1%
5	5,570,315	893,318	2%	7%
1	5,804,712	858,628	2%	3%

Table 6: Summary of results.

CELL SIZE	EXPERIMENTAL RESPONSE	MEAN	STANDARD DEVIATION	P-VALUE
0.5mm	Volume [mm ³]	1,401,218	77,703	0.756
	Area [mm ²]	424,781	13,627	0.354
1.0mm	Volume [mm ³]	1,413,867	86,727	0.268
	Area [mm ²]	283,804	16,236	0.275
2.0mm	Volume [mm ³]	5,705,143	402,076	0.629
	Area [mm ²]	833,286	54,679	0.374

4. DISCUSSION

There are a number of studies on the effects of pore size on the mechanical properties of aluminum, titanium and magnesium and their alloy foams. It was found that the relationship between the compressive strength and the porosities is completely linear relation beyond the effect of pore size distributions on the mechanical properties [11]. Furthermore, it is worth noting that both the foam structure and the pore morphology depend on the fabrication method, utilized during manufacturing of the foams, which in turn determine the mechanical properties [12].

Several authors had shown limited number of methods to produce open cellular structures that allow obtaining uniform pore distribution [12]. In order to probe complex porous structures, high resolution X-ray computed tomography (XCT) or MRI techniques have been used in recent years. Bekoz *et al* [12], calculated the area of each pore on the SEM image and measured the pores size, shape and size distribution using Clemex Vision PE commercial image-analyzer software.

Saadatfar *et al* [13], used tomographic imaging technique to distinguish small changes in density, pore size distribution and pore geometry/topology of samples of different precursor sizes and geometries, made under gravity.

In this study, taking into account that usually cellular materials having small bubbles with uniform size and spherical shape are guarantee for better mechanical properties, it was found that despite of irregular morphology of pores; the high uniformity in pores distribution obtained with the evaluated process and the presence of numerous channels between the cells, makes CDP foams a sort of materials with outstanding mechanical properties.

5. CONCLUSIONS

The manufacturing and reconstruction process guarantee to obtain physical and virtual foams with a homogenous pore distribution.

It is widely accepted that foams with a uniform pore distribution and defects free, are desirable. It is worth noting that foams made by Casting - Dissolution Process provide uniform pore distribution in an aluminum alloy foam. Furthermore, all sections of metal foams are a representative sample of the entire volume and make useful to evaluate mechanical properties of the foam using computational numerical models, as it was proved by statistical method.

Due to the destructive test disturb the cell structure, 3D image analysis is a worthy method to extract a range of geometrical and topological properties including porosity, pore volume, size distribution and cell connectivity, which are directly measured on the images.

6. BIBLIOGRAPHY

- [1] GRISHIN, A. *A Mesh-Free Finite Element Solution for Unilateral Contact Problems*, Ph.D, Arizona State University, Arizona, United States, 2010.
- [2] JARILLO, J.M. *Modelización del comportamiento mecánico de una espuma metálica*, M. Sc. Universidad Carlos III de Madrid, Madrid, España. 2009.
- [3] YOUSSEF, S., MAIRE, E., GAERTNER, R. "Finite element modelling of the actual structure of cellular materials determined by X-ray tomography", *Acta Mater.*, v. 53, n 3, pp. 719–730, Feb. 2005.

- [4] SMITH, B.H., SZYNISZEWSKI, S., HAJJAR, J.F., *et al.*, “Steel foam for structures: A review of applications, manufacturing and material properties”, *Journal of Constructional Steel Research*, v 71, pp. 1–10, Apr. 2012.
- [5] BANHART, J. “Manufacture, characterisation and application of cellular metals and metal foams”. *Progress in Materials Science*, v 46, pp. 559-632, Jan 2001.
- [6] PARVANI, A.M., SAADATFAR, M., PANJEPOUR, M., *et al.*, “The effects of manufacturing parameters on geometrical and mechanical properties of copper foams produced by space holder technique”, *Materials & Design.*, v. 53, pp. 681–690, Jan. 2014.
- [7] SURACE, R., FILIPPIS, L., LUDOVICO, A., *et al.*, “Influence of processing parameters on aluminium foam produced by space holder technique”, *Materials & Design.*, v. 30, n. 6, pp. 1878–1885, Jun. 2009.
- [8] ZHAO, Y.Y., FUNG, T., ZHANG, L.P., *et al.*, “Lost carbonate sintering process for manufacturing metal foams”, *Scripta Materialia.*, v. 52, n. 4, pp. 295–298, Feb. 2005.
- [9] MAIRE, E., FAZEKAS, A., SALVO, L., *et al.*, “X-ray tomography applied to the characterization of cellular materials. Related finite element modeling problems”, *Composites Science and Technology.*, v. 63, n. 16, pp. 2431–2443, Dec. 2003.
- [10] BOCK, J., JACOBI, A.M., “Geometric classification of open-cell metal foams using X-ray micro-computed tomography”, *Materials Characterization.*, v. 75, pp. 35–43, Jan. 2013.
- [11] WANG, X., LI, J., HU, R., *et al.*, “Mechanical properties of porous titanium with different distributions of pore size,” *Trans. Nonferrous Met. Soc. China*, v. 23, no. 8, pp. 2317–2322, Aug. 2013.
- [12] BEKOZ, N., OKTAY, E. “Mechanical properties of low alloy steel foams: Dependency on porosity and pore size,” *Mater. Sci. Eng. A*, v. 576, pp. 82–90, Aug. 2013.
- [13] SAADATFAR, M., GARCIA-MORENO, F., HUTZLER, S., *et al.*, “Imaging of metallic foams using X-ray micro-CT,” *Colloids Surfaces A Physicochem. Eng. Asp.*, vol. 344, no. 1–3, pp. 107–112, Jul. 2009.
- [14] JAKUBOWICZ, J., ADAMEK, G., PAŁKA, K., *et al.*, “Micro-CT analysis and mechanical properties of Ti spherical and polyhedral void composites made with saccharose as a space holder material”, *Mater. Charact.*, v. 100, pp. 13–20, Feb. 2015